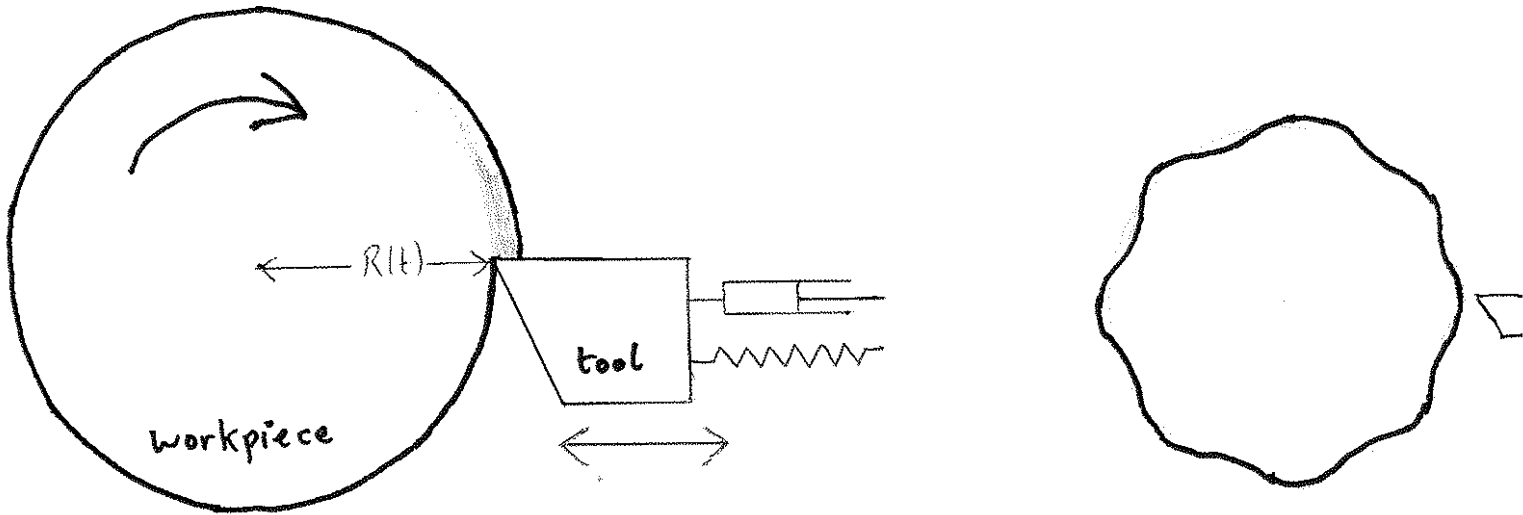


Machining vibrations (chatter)



Angular velocity = Ω radians/sec.

time for one revolution = $\frac{2\pi}{\Omega}$

Suppose d_0 = desired steady state chip thickness

Need to move tool inwards such that

$$R(t) = R_0 - \frac{d_0 \Omega}{2\pi} t$$

↑
initial radius

But the tool may vibrate. Suppose that, in fact,

$$R(t) = R_0 - \frac{d_0 \Omega t}{2\pi} - y(t)$$

Then the chip thickness $d(t)$ at time t is

$$d(t) = \left[R_0 - \frac{d_0 \Omega}{2\pi} \left(t - \frac{2\pi}{\Omega} \right) - y \left(t - \frac{2\pi}{\Omega} \right) \right] - \left[R_0 - \frac{d_0 \Omega t}{2\pi} - y(t) \right]$$

$$\boxed{d(t) = d_0 + y(t) - y(t - \tau)}$$

$$\boxed{\tau = \frac{2\pi}{\Omega}}$$

Consider forces on tool:

$$m \frac{d^2 y}{dt^2} = \underbrace{(\text{force from spring})}_{\text{Hooke's law}} - \underbrace{(\text{cutting force})}_{\text{depends on chip thickness } d(t)}$$

In steady state, with $y=0$,

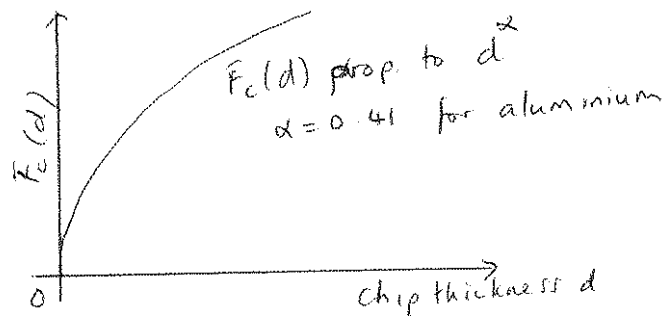
Cutting force on tool = force from spring

$$F_c(d_0) = k l_0$$

Spring constant Compression in equilibrium

Cutting force, depends on chip thickness

Experiments suggest:



In vibration:

$$m \frac{d^2 y}{dt^2} = \underbrace{k(l_0 - y(t))}_{\text{force from spring}} - \underbrace{F_c(d(t))}_{\text{cutting force}}$$

$$\approx k(l_0 - y(t)) - (F_c(d_0) + (d(t) - d_0) F_c'(d_0))$$

$$m \frac{d^2 y}{dt^2} + k y(t) = -(y(t) - y(t - \tau)) F_c'(d_0)$$

Including a damping term:

$$m \frac{d^2 y}{dt^2} + \gamma \frac{dy}{dt} + k y(t) + (y(t) - y(t - \tau)) F_c'(d_0) = 0$$

$$y(t) = e^{\lambda t} \Rightarrow$$

$$m\lambda^2 + \gamma\lambda + k + F_c'(d_0)(1 - e^{-\lambda\tau}) = 0$$

Thm: if $\Omega\gamma > 2\pi F_c'(d_0)$ then all roots of the characteristic eqn satisfy $\text{Re}\lambda < 0$, so that $\lim_{t \rightarrow \infty} y(t) = 0$.

Proof note $\Omega\gamma > 2\pi F_c'(d_0) \Leftrightarrow \gamma > F_c'(d_0)\tau$

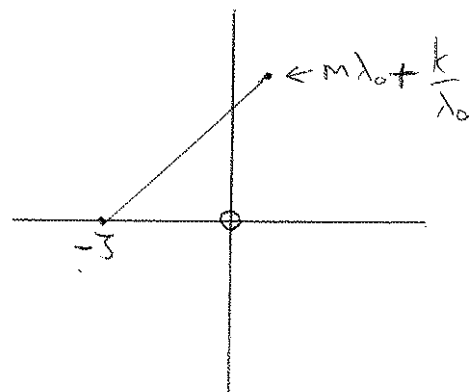
Suppose \exists a root λ_0 with $\text{Re}\lambda_0 \geq 0$.

$$\begin{aligned} |m\lambda_0^2 + \gamma\lambda_0 + k| &= F_c'(d_0) |1 - e^{-\lambda_0\tau}| \\ &= F_c'(d_0) \left| \lambda_0 \int_0^\tau e^{-\lambda_0 s} ds \right| \\ &\leq F_c'(d_0) |\lambda_0| \tau \quad \text{since } \text{Re}\lambda_0 \geq 0. \end{aligned}$$

$$\therefore \left| m\lambda_0 + \frac{k}{\lambda_0} + \gamma \right| \leq F_c'(d_0)\tau$$

distance between $m\lambda_0 + k/\lambda_0$ and $-\gamma$

But $\text{Re}\lambda_0 \geq 0 \Leftrightarrow \text{Re} m\lambda_0 + \frac{k}{\lambda_0} \geq 0$



\therefore distance is always $\geq \gamma$

$\therefore \gamma \leq F_c'(d_0)\tau$ contradiction.

\therefore to avoid chatter: can speed up rotation (increase Ω) or increase damping (increase γ).